

A High Current Proton Linac with 352 MHz SC Cavities

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Abstract

A proposal for a 10-120 mA proton linac employing superconducting beta-graded, CERN type, four cell cavities at 352 MHz is presented.

The high energy part (100 MeV-1 GeV) of the machine is split in three β -graded sections, and transverse focusing is provided via a periodic doublet array. All the parameters, like power in the couplers and accelerating fields in the cavities, are within the state of the art, achieved in operating machines.

A first stage of operation at 30 mA beam current is proposed, while the upgrade of the machine to 120 mA operation can be obtained increasing the number of klystrons and couplers per cavity. The additional coupler ports, up to four, will be integrated in the cavity design. Preliminary calculations indicate that beam transport is feasible, given the wide aperture of the 352 MHz structures.

A capital cost of less than 100 M\$ at 10 mA, reaching up to 280 M\$ for the 120 mA extension, has been estimated for the superconducting high energy section (100 MeV-1 GeV).

The high efficiency of the proposed machine, reaching 50% at 15 mA, makes it a good candidate for proposed nuclear waste incineration facilities and Energy Amplifier studies[1, 2].

Choice of the 352 MHz Frequency

Our design is based mainly on the choice of a low RF frequency for the SC linac. A wide experience in the design, construction and operation of 352 MHz cavities and RF systems is available at CERN[3]. The 352 MHz frequency at moderate gradient operation (around 5 MV/m) allows for large geometrical irises and lower beam current densities. A critical issue for such a machine will be the control of the beam halo growth[4], and the choice of a low frequency allows to lower both the space charge tune depression and the ratio of the beam (core) size with respect to the beam line aperture.

Another important issue, the future availability of several 1.3 MW CW klystrons of the CERN LEP RF system, that will be decommissioned before year 2000, gives an economical impulse for the investigation of a scheme based on the LEP 352 MHz frequency. Moreover, we have also to take into account the experience of several European companies for cavities production and the cavity tooling machines already available at the companies[3].

In our view the development of new β -graded structures[5, 2], with up to four coupler ports, at 352 MHz could allow to reach a beam current of 120 mA employing present technological RF components (simply by incrementing the number of klystrons

and couplers/cavity, limiting the power per coupler to approximately 200 kW).

In the following we present a preliminary parameter set for the high energy part (100 MeV-1 GeV) of the machine, as presented to C. Rubbia in the framework of a possible INFN collaboration to the Energy Amplifier and waste transmutation project. The low energy part should be composed of two sections: an RFQ[2] (up to ≈ 7 MeV) and a conventional DTL linac (up to ≈ 100 MeV). This design has been recently included as the candidate for the high energy accelerator section of the Energy Amplifier proposal[6], and work is in progress for a full optimization of the optics and for the development of the RF cavities.

The β -graded structures for the high energy section

We have chosen to cover the energy range from 100 MeV to 1 GeV with three different families of β -graded four cell cavities at 352 MHz, with cell length defined as $L_{\text{cell}} = \bar{\beta}\lambda_{\text{RF}}/2$. Four cell cavities have been chosen in order to reduce the number of cavities and the physical structure length, that has to include cut-off tubes, coupler and HOM ports.

This choice of three energy ranges (and consequently of three $\bar{\beta}$ values for the different sections) allows to keep the transit time factor of a particle in each cavity always greater than 0.9, along the whole machine.

The main characteristics of the cavities in each section are given in Table 1.

Energy (MeV)	$\bar{\beta}$	L_{active} (m)	L_{FIDO} (m)
100–185	0.47	0.800	7.5
185–360	0.60	1.022	8.4
360–1000	0.76	1.294	9.5

Table 1: Energy range, design $\bar{\beta}$, active length and length of the focussing period, for the three families of 4 cell cavities.

The energy gain in each cavity is given by:

$$\Delta T_{\text{cav}} (\text{MeV}) = L_{\text{active}}(m) E_{\text{acc}} (\text{MV}/m) g \left(\frac{\bar{\beta}}{\beta} \right) \cos(\phi_{\text{RF}})$$

where $L_{\text{active}} = N L_{\text{cell}}$ is the active cavity length (in Table 1), E_{acc} is the accelerating field in the cavity, $g(\bar{\beta}/\beta)$ is the transit time factor of the cavity, depending on the design $\bar{\beta}$ and the actual beam β , and ϕ_{RF} is the operating RF phase.

In our design, considering the requirement of phase stability, we have chosen $\phi_{\text{RF}} = -30^\circ$, and $g > 0.9$ all over the machine.

The role of the transit time factor g can be seen in Figure 1, where we plot the energy gain of each cavity along the machine. Here we chose a constant E_{acc} in each section (the values are given in Table 2); as an alternative approach one can individually set the cavity gradients to provide a constant energy gain in the sections.

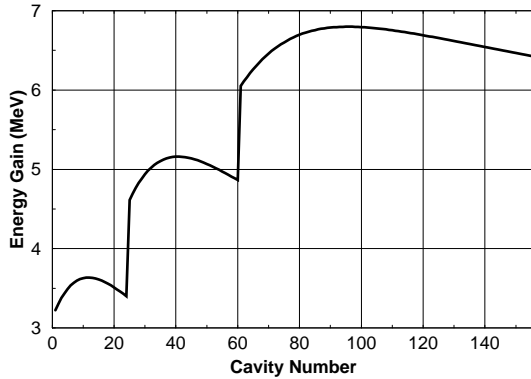


Figure 1: Energy gain along the three linac sections, as a function of the cavity number, keeping the nominal accelerating gradient fixed in each section (see text for details).

The basic accelerating cell of each linac section consists of one cryomodule containing four cavities, transverse focusing is provided by quadrupole doublets every cryomodule.

Focusing Structure

The focusing structure is a FIDA cell, where the beam acceleration is provided by four RF cavities, in one cryomodule, between successive quadrupole doublets, as seen in Figure 2. The possible use of quadrupole triplets to allow for “rounder” beams will also be considered.

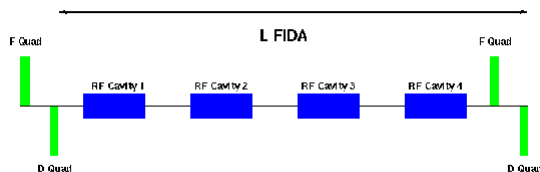


Figure 2: Focusing structure of the linac.

The three sections of the linac have different cell lengths. The active cavity length and the corresponding lattice periodicity in the three sections are indicated in Table 1.

The quadrupole integrated field GI ranges from 1 to 3.5 T along the machine, hence it is possible to place warm normal conducting quadrupoles between the cryomodules.

For this reference design the zero current maximal phase advance per cell has been set to 90° , although a value close to 60° or 72° should be more appropriate. In the first unit of the first section there is a strong longitudinal phase advance and a reduction of E_{acc} will be investigated.

Preliminary calculations with the linear space charge code TRACE-3D[7] in the current range of 10-120 mA show that beam transport with a beam radius/aperture ratio in the range 10–50 along the machine is possible.

Section details

In Table 2 we report the main characteristics of the three sections of the high energy part of the linac, including RF power distribution. The maximum RF power in the couplers is approximately 200 kW, the current upgrade would require the insertion of additional couplers (up to four) in each cavity. The four coupler ports should be integrated from the beginning in the cavity design.

	S. 1	S. 2	S. 3
N. of structures	24	36	96
$\bar{\beta}$	0.47	0.60	0.76
E_{acc} (MV/m)	5.2	5.8	6.0
Section length (m)	45	76	226
10 mA beam current			
RF Power/section (MW)	0.85	1.81	6.35
RF Power/cavity (kW)	35.4	50.3	66.1
couplers/cavity	1	1	1
Klystron/section	1	2	6
120 mA beam current			
RF Power/section (MW)	10.2	21.72	76.2
RF Power/coupler (kW)	212	201	198
couplers/cavity	2	3	4
Klystron/section	≈ 10	≈ 20	≈ 80

Table 2: Section details.

A total of 156 cavities and 350 m of physical length are required for the three sections of the superconducting linac, in this reference design. These two numbers could slightly increase in the final design, in order to: decrease the cavity gradient, employ quadrupole triplets focusing, include beam diagnostic elements inside the cryomodules or matching elements between sections.

Cost of the linac, and efficiency considerations

The capital cost of the superconducting linac, excluding the RF power costs, is approximately 72.5 M\$, and the cost breakdown is indicated in Table 3.

Estimated RF Capital Cost

Assuming, 1.5 M\$ per klystron (1.3 MW, CW with power supplies) and 50 k\$ per coupler (including the RF distribution), in Figure 3 we plot the total capital cost of the linac (including the RF system), and the total capital cost per MW of beam power, as a function of the beam current (in mA).

Overall Linac Efficiency vs. Beam Current

Assuming a klystron efficiency of 58%, a refrigeration power of approximately 2.5 MW and a contingency power of 1 MW dedicated to the ancillary components of the linac, the overall effi-

Item	Number	M\$
Cavities (with tuners)	156	39.0
Quadrupoles	78	3.1
RF Controls	156	4.2
Vacuum Pumps	40	1.0
Vacuum Valves	78	1.0
Cryostats	39	8.0
Beam Monitors	80	0.8
Controls	1	3.0
Cryoplant Cost (8 kW @ 4.2 K)	1	8.9
Ancillary Equip. (350 m)		3.5
Total Cost		72.5

Table 3: Capital cost of the SC linac.

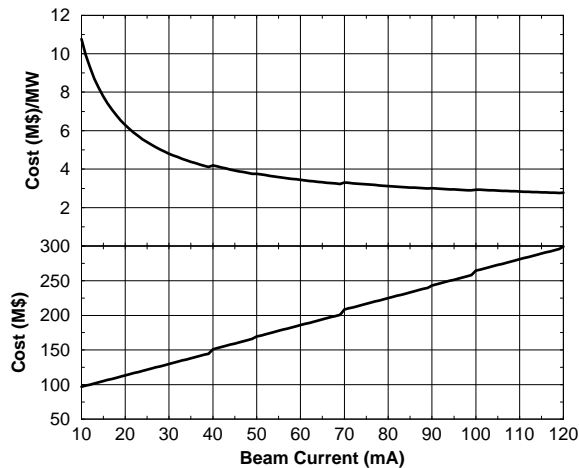


Figure 3: Lower curve: Linac total capital cost (in M\$, including RF system). Upper curve: Total cost per MW of beam power vs. beam current (mA).

ciency of the machine as a function of the beam current is presented in Figure 4. Note that 50% plug efficiency is reached at 15 mA operation. The operation at the full 120 mA current would allow to reach nearly the nominal klystron efficiency.

Conclusions

A preliminary study for a low frequency, high current superconducting proton linac for nuclear waste incineration and energy amplifier applications has been proposed. The machine operates at the 352 MHz of the LEP RF system with three sections of β -graded superconducting cavities.

Preliminary calculations indicate that beam transport at high current is possible, and further studies to address cavity design, both from the electromagnetic and the engineering point of view, and beam halo formation are in the starting phase.

The choice of the RF frequency and of the machine parameters provides a very good plug efficiency at high beam current, a crucial issue for the proposed applications.

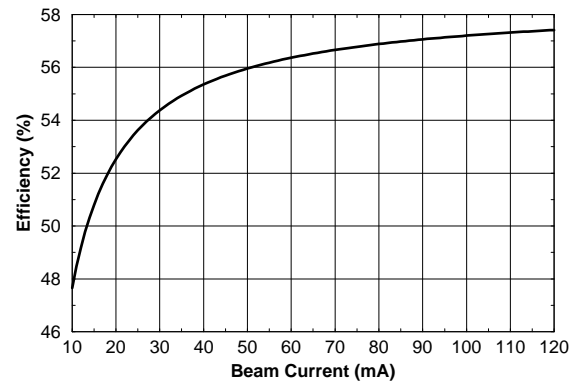


Figure 4: Overall linac plug efficiency vs. beam current (mA)

Acknowledgements

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